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INVENTION TITLE: METHOD OF AND APPARATUS FOR MEASUREMENT
AND CONTROL OF A GAS CLUSTER ION BEAM

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Sir:

Your applicant(s) named above hereby petition(s) for grant of a utility patent to him (them) or any assignee(s) of record, at the time of issuance, for an invention, more particularly described in the following specification and claims, with the accompanying drawings, verified by the accompanying Declaration and entitled:

**METHOD OF AND APPARATUS FOR MEASUREMENT AND CONTROL
OF A GAS CLUSTER ION BEAM**

Cross Reference To Related Patent Applications

[0001] This application claims priority of U. S. Provisional Application Serial No. 60/442,854 entitled "Method And Apparatus For Measurement And Control Of A Gas Cluster Ion Beam", filed January 27, 2003, the contents of which are incorporated herein by reference.

Background Of The Invention

[0002] The present invention relates generally to the measurement and control of characteristics of a cluster ion beam and, more particularly, to measuring and/or controlling the average charge state, average cluster ion mass, and/or average cluster ion energy of cluster ions in a gas cluster ion beam.

[0003] The use of a cluster ion beam for processing surfaces is known (see for example, US patent 5,814,194, Deguchi et al., incorporated herein by reference) in the art. For purposes of this discussion, gas clusters are nano-sized aggregates of materials that are gaseous under conditions of standard temperature and pressure. Such gas clusters typically are comprised of aggregates of from a few to several thousand molecules loosely bound to form the cluster. The clusters can be ionized by electron bombardment or other means, permitting them to be formed into directed beams of controllable energy. Such ions each typically carry positive charges of $q \cdot e$ (where e is the electronic charge and q is an integer of from one to several representing the charge state of the cluster ion). Non-ionized clusters may also exist within a cluster ion beam. The larger sized cluster ions are often the most useful because of their ability to carry substantial energy per cluster ion, while yet having only modest energy per molecule. The clusters disintegrate on impact, with each individual molecule carrying only a small fraction of the total cluster ion energy. Consequently, the impact effects of large cluster ions are substantial, but are limited to a very shallow surface region. This makes cluster ions effective for a variety of surface modification processes, without the tendency to produce deeper subsurface damage characteristic of conventional monomer ion beam processing.

[0004] Means for creation of and acceleration of such gas cluster ion beams (GCIBs) are described in the reference (US 5,814,194) previously cited. Presently available cluster ion sources produce clusters ions having a wide distribution of sizes, N (where N = the number of molecules in each cluster ion - in the case of monatomic gases like argon, an atom of the monatomic gas will be referred to as a molecule and an ionized atom of such a monatomic gas will be referred to as a molecular ion - or simply a monomer ion - throughout this discussion).

[0005] Many useful surface processing effects can be achieved by bombarding surfaces with GCIBs. These processing effects include, but are not necessarily limited to, cleaning, smoothing, etching, and film growth. There is need for improved diagnostic measurements to predict and control the gas cluster ion beam physics that affect processing rates of surfaces and hence permit these rates to be optimized. The fundamentals of GCIB-surface interactions are individual cluster ions impacting a surface, moving and ejecting material by direct sputtering and/or through melting and evaporation, creating nano-scale craters of various depths and diameters. GCIB craters can be on the on the scale of tens to hundreds of Angstroms, and depend on cluster ion mass and velocity. The nature of the craters formed (and thus the surface processing characteristics) by a GCIB depends on the mass of the cluster ions and their impact velocity.

[0006] Cluster ion velocity may be measured using time-of-flight techniques (as taught in U.S. Patent Application Publications 2002-0036261A1, Dykstra, Jerald P., and 2002-0070361A1, Mack, *et al.*, for example, which are incorporated herein by reference). Also, by a variety magnetic and electrostatic measurement techniques sensitive to the mass/charge state ratio (m/q), the momentum, energy and mass of ionized clusters can be determined, when using ionization conditions such that the ions are predominantly singly charged, thus assuring that q was known to be approximately one. Additionally, it is known that techniques exist for measuring average mass/charge state ratio, $\left(\frac{m}{q}\right)_{average}$, or can be based on existing techniques (as taught in U.S. Patent Application Publication 2001-0054686A1, Torti. *et al.*, for example, incorporated by reference).

[0007] In many cases, it is found that in order to achieve industrially practical throughputs in GCIB processing, GCIB currents on the order of hundreds to thousands of microamps are required. Recent efforts to increase the intensity and ionization of GCIBs are producing additional higher charge state clusters ($q > 1$). When ionization is performed by electron bombardment, ionization is produced by random electron impacts. In order to produce a high ratio of ionized to non-ionized clusters, the electron impact probability must be high and the resulting charge state distribution follows approximately Poisson statistics, with the approximate probability, $P(q)$, of charge state q given by:

$$P(q) = \frac{\bar{q}^q}{q!} e^{-\bar{q}}, \quad (\text{Eqn. 1})$$

where \bar{q} is the average ionized cluster charge state after leaving the ionizer. Thus an ionized cluster beam with a highly ionized fraction will also be a multiply charged beam. For example, theoretically the average cluster charge state of a GCIB beam where 95% of the clusters are ionized would be 3, with more than 8% of the beam in charge states 6 and higher. However, such highly charged clusters can fragment, resulting in a different charge state distribution. The interaction of the cluster ions with residual gas in the vacuum system can also cause charge exchange reactions and cluster ion fragmentation and so in a practical beam, the precise charge state is not readily predicted. The existence of high charge state clusters cannot be determined using present instrumentation such as magnetic spectrometers, electrostatic spectrometers, RF quadrupole mass spectrometers, time-of-flight, retarding potential mass spectrometers, and pressure gauge measurements, all of which measure either m/q or the energy/charge state ratio, E/q . It should be noted that for ionized cluster m/q on the order of 10000 AMU or less, it is possible to resolve different charge state families in the m/q spectra but this is not practical for more massive cluster ions where m/q states cannot be practically resolved or overlap. Other methods have been used to determine these parameters for very-large very-highly-charged ($q > 1000$) molecules produced by electro-spray techniques, and also for the case of highly-charged

atoms in the solar wind or electrostatically accelerated dust particles. These techniques are not applicable to GCIBs because, for the former case, the charge states are too low, and with respect to the latter technique, because the cluster ion's collision energy is nearly all deposited thermally and hence cannot be detected using practical known methods. Thus, improved methods and apparatus are needed to measure and control m , q and E of these cluster ions.

[0008] It is therefore an object of this invention to provide methods and apparatus for measuring the average charge state \bar{q} of a cluster ion beam.

[0009] It is a further object of this invention to provide methods and apparatus for measuring average mass \bar{m} and/or average energy \bar{E} of energetic ionized clusters in a beam.

[0010] Another object of this invention is to provide an improved method and apparatus for measuring and controlling the properties of a gas cluster ion beam in a GCIB processing system for improved GCIB processing of a workpiece.

Summary Of The Invention

[0011] The objects set forth above as well as further and other objects and advantages of the present invention are achieved by the embodiments of the invention described hereinbelow.

[0012] In a first embodiment, the present invention provides a method involving separate measurements of average energy per charge $\left(\frac{E}{q}\right)_{average}$, average velocity \bar{v} , and average charge state \bar{q} on a sample of cluster ion beam. The average energy per charge is measured using an electrostatic spectrometer, and the velocity is measured using time-of-flight. The average charge state \bar{q} is measured and used in combination with the other measurements to determine averages of m and E for the ionized cluster distribution. The average charge state is calculated by measuring the flow rate of particles (clusters), Γ , using a fast particle counter and by measuring the electrical beam current, I , using a current sensor, preferably a faraday cup, for a small sample of the ion beam. The ratio of electrical current to particle flow (according to Eqn. 2 below) yields the cluster average charge state, \bar{q} measurement. This average charge state measurement is

combined with the electrostatic spectrometer measurements of $\left(\frac{E}{q}\right)_{average}$ to determine the average cluster ion energy, and with time-of-flight measurements of average velocity, \bar{v} , to determine average mass, \bar{m} , as described in **Eqn. 2**, **Eqn. 3**, and **Eqn. 5** below.

[0013] In a second embodiment, the present invention provides a method of making measurements of average mass per charge $\left(\frac{m}{q}\right)_{average}$, of the beam and of average energy per charge $\left(\frac{E}{q}\right)_{average}$, and average charge state \bar{q} on a sample of the cluster ion beam. The average energy per charge is measured using an electrostatic spectrometer, and the average mass per charge is measured using a pressure-charge sensor. The average charge state \bar{q} is measured and used in combination with the other measurements to determine averages of m and E for the ionized cluster distribution. As in the first embodiment, the average charge state is measured by measuring the flow rate of particles (clusters), Γ , using a fast particle counter and by measuring the electrical beam current, I , using a current sensor, preferably a faraday cup for a small sample of the ion beam. The ratio of electrical current to particle flow (according to **Eqn. 2**) yields the cluster average charge state, \bar{q} measurement. This average charge state measurement is combined with the electrostatic spectrometer measurements of $\left(\frac{E}{q}\right)_{average}$ to determine the average cluster ion energy, and with average mass per charge, $\left(\frac{m}{q}\right)_{average}$, measurements to determine average mass, \bar{m} , as described in **Eqn. 2**, **Eqn. 3**, and **Eqn. 4** below.

[0014] In **Eqn. 2**, α and β are the detection efficiencies for the current and particle detectors respectively.

$$\bar{q} = \frac{\alpha I}{\beta e \Gamma} \quad (\text{Eqn. 2})$$

$$\bar{E} = \bar{q} \left(\frac{E}{q} \right)_{\text{average}} \quad (\text{Eqn. 3})$$

$$\bar{m} = \bar{q} \left(\frac{m}{q} \right)_{\text{average}} \quad (\text{Eqn. 4})$$

$$\bar{m} = \frac{2\bar{E}}{\bar{v}^2} \quad (\text{Eqn. 5})$$

Brief Description Of The Drawing

[0015] For a better understanding of the present invention, together with other and further objects thereof, reference is made to the accompanying figures and detailed description, wherein:

[0016] **Figure 1** is a schematic showing the basic elements of a prior art GCIB processing apparatus that uses an electrostatically scanned beam;

[0017] **Figure 2** is a schematic showing the basic elements of a GCIB processing apparatus that uses a stationary beam with mechanical scanning of the workpiece;

[0018] **Figure 3A** is a schematic showing a first embodiment of the apparatus for making the beam measurements of the invention, wherein is depicted a case for an analyzer voltage of zero;

[0019] **Figure 3A** is a schematic showing a first embodiment of the apparatus for making the beam measurements of the invention, wherein is depicted a case for a non-zero analyzer voltage;

[0020] **Figure 4** is a schematic showing a first embodiment of the apparatus for making the beam measurements of the invention configured for measuring the current I of a sample of the beam;

[0021] **Figure 5** is a schematic showing a first embodiment of the apparatus for making the beam measurements of the invention, illustrating beam gating for time-of-flight measurements on a sample of the beam;

[0022] **Figure 6** is a schematic showing a first embodiment of the apparatus of the invention for making the beam measurements, with improvements removed from the beam path to permit measurement of the current of the entire beam;

[0023] **Figure 7** is a schematic of a second embodiment of the apparatus of the invention for making the beam measurements;

[0024] **Figure 8** is a schematic showing a first embodiment of the apparatus of the invention for making the beam measurements, with improvements removed from the beam and a workpiece inserted into the beam for processing;

[0025] **Figure 9** is a schematic showing a GCIB processing apparatus according to the first embodiment of the invention;

[0026] **Figure 10** is a schematic showing a GCIB processing apparatus according to the first embodiment of the invention, with the beam measurement apparatus removed from the beam to allow workpiece processing; and

[0027] **Figure 11** is a schematic showing the improved GCIB processing apparatus according to the second embodiment of the invention, with the beam measurement apparatus removed from the beam to allow workpiece processing.

Detailed Description Of The Preferred Embodiments

[0028] **Figure 1** shows a schematic of the basic elements of a typical configuration for a GCIB processor **100**, which may be described as follows: a vacuum vessel **102** is divided into three communicating chambers, a source chamber **104**, an ionization/acceleration chamber **106**, and a processing chamber **108**. The three chambers are evacuated to suitable operating pressures by vacuum pumping systems **146a**, **146b**, and **146c**, respectively. A condensable source gas **112** (for example argon or N₂) stored in a gas storage cylinder **111** is admitted under pressure through gas metering valve **113** and gas feed tube **114** into stagnation chamber **116** and is ejected into the substantially lower pressure vacuum through a properly shaped nozzle **110**. A supersonic gas jet **118** results. Cooling, which results from the expansion in the jet, causes a portion of the gas jet **118** to condense into clusters, each consisting of from several to several thousand weakly

bound atoms or molecules. A gas skimmer aperture **120** partially separates the gas molecules that have not condensed into a cluster jet from the cluster jet so as to minimize pressure in the downstream regions where such higher pressures would be detrimental (e.g., ionizer **122**, high voltage electrodes **126**, and processing chamber **108**). Suitable condensable source gases **112** include, but are not necessarily limited to argon, nitrogen, carbon dioxide, oxygen, and other gases.

[0029] After the supersonic gas jet **118** containing gas clusters has been formed, the clusters are ionized in an ionizer **122**. The ionizer **122** is typically an electron impact ionizer that produces thermoelectrons from one or more incandescent filaments **124** and accelerates and directs the electrons causing them to collide with the gas clusters in the gas jet **118**, where the jet passes through the ionizer **122**. The electron impact ejects electrons from the clusters, causing a portion the clusters to become positively ionized. A set of suitably biased high voltage electrodes **126** extracts the cluster ions from the ionizer, forming a beam, then accelerates them to a desired energy (typically from 1 keV to several tens of keV) and focuses them to form a GCIB **128** having a GCIB axis **129**. Filament power supply **136** provides filament voltage V_f to heat the ionizer filament **124**. Anode power supply **134** provides anode voltage V_A to accelerate thermoelectrons emitted from filament **124** to cause them to irradiate the cluster containing gas jet **118** to produce ions. Extraction power supply **138** provides extraction voltage V_E to bias a high voltage electrode to extract ions from the ionizing region of ionizer **122** and to form a GCIB **128**. Accelerator power supply **140** provides acceleration voltage V_{Acc} to bias a high voltage electrode with respect to the ionizer **122** so as to result in a total GCIB acceleration energy equal to V_{Acc} electron volts (eV). One or more lens power supplies (**142** and **144** shown for example) may be provided to bias high voltage electrodes with focusing voltages (V_{L1} and V_{L2} for example) to focus the GCIB **128**.

[0030] A workpiece **152**, which may be a semiconductor wafer or other workpiece to be processed by GCIB processing, is held on a workpiece holder **150**, disposed in the path of the GCIB **128**. Since most applications contemplate the processing of large workpieces with spatially uniform results, a scanning system is desirable to uniformly scan the GCIB **128** across large areas to produce spatially homogeneous results. Two pairs of orthogonally oriented

electrostatic scan plates **130** and **132** can be utilized to produce a raster or other scanning pattern across the desired processing area. When beam scanning is performed, the GCIB **128** is converted into a scanned GCIB **148**, which scans the entire surface of workpiece **152**.

[0031] **Figure 2** shows a schematic of the basic elements of a prior art mechanically scanning GCIB processing apparatus **200** having a stationary beam with a mechanically scanned workpiece **152**, and having a conventional faraday cup for beam measurement and a conventional thermionic neutralizer. GCIB generation is similar to as is shown in **Figure 1**, but in the mechanically scanning GCIB processing apparatus **200** of **Figure 2**, the GCIB **128** is stationary (not scanned) and the workpiece **152** is mechanically scanned through the GCIB **128** to distribute the effects of the GCIB **128** over a surface of the workpiece **152**. An X-scan actuator **202** provides linear motion of the workpiece holder **150** in the direction of X-scan motion **208** (into and out of the plane of the paper). A Y-scan actuator **204** provides linear motion of the workpiece holder **150** in the direction of Y-scan motion **210**, which is typically orthogonal to the X-scan motion **208**. The combination of X-scanning and Y-scanning motions moves the workpiece **152**, held by the workpiece holder **150** in a raster-like scanning motion through GCIB **128** to cause a uniform irradiation of a surface of the workpiece **152** by the GCIB **128** for uniform processing of the workpiece **152**. The workpiece holder **150** disposes the workpiece **152** at an angle with respect to the GCIB axis **129** of the GCIB **128** so that the GCIB **128** has an angle of beam incidence **206** with respect to the workpiece **152** surface. The angle of beam incidence **206** may be 90 degrees or some other angle, but is typically 90 degrees or very near 90 degrees. During Y-scanning, the workpiece **152** held by workpiece holder **150** moves from the position shown to the alternate position "A", indicated by the designators **152A** and **150A** respectively. Notice that in moving between the two positions, the workpiece **152** is scanned through the GCIB **128** and in both extreme positions, is moved completely out of the path of the GCIB **128** (over-scanned). Though not shown explicitly in **Figure 2**, similar scanning and over-scan is performed in the (typically) orthogonal X-scan motion **208** direction (in and out of the plane of the paper). A total beam current sensor **218** is disposed beyond the workpiece holder **150** in the path of the GCIB **128** so as to intercept a sample of the total GCIB beam current I_T of

GCIB 128 when the workpiece holder 150 is scanned out of the path of the GCIB 128. The beam current sensor 218 is typically a faraday cup or the like, closed except for a beam-entry opening, and is affixed to the wall of the vacuum vessel 102 with an electrically insulating mount 212. A controller 220, which may be a microcomputer based controller connects to the X-scan actuator 202 and the Y-scan actuator 204 through electrical cable 216 and controls the X-scan actuator 202 and the Y-scan actuator 204 so as to place the workpiece 152 into or out of the GCIB 128 and to scan the workpiece 152 uniformly relative to the GCIB 128 to achieve uniform processing of the workpiece 152 by the GCIB 128. Controller 220 receives the sampled beam current collected by the beam current sensor 218 by way of lead 214 and thereby monitors the GCIB and controls the GCIB dose received by the workpiece 152 by removing the workpiece 152 from the GCIB 128 when a predetermined desired dose has been delivered.

[0032] Figures 3A and 3B show schematics of a first embodiment of a GCIB measurement apparatus 300 for making the beam measurements of a GCIB 128 in accordance with the present invention. Figure 3A depicts a case for an analyzer voltage of zero and Figure 3B depicts a case for a non-zero analyzer voltage. The GCIB measurement apparatus 300 is intended to be situated (with the exception, optionally, of some or all supporting electronic circuits, power supplies, and controls) within the vacuum vessel 102 (Figure 2) of a GCIB processing apparatus 200 (Figure 2) having an unscanned GCIB 128, like that shown in Figure 2, for example. The GCIB measurement apparatus 300 comprises a GCIB attenuation subsystem, a GCIB collimation subsystem, a GCIB switching subsystem, a GCIB energy spectrum measuring subsystem, a GCIB particle flow measurement subsystem, a GCIB current measurement subsystem, a GCIB time-of-flight measurement system, repositioning actuators for repositioning various elements with respect to the gas cluster ion beam being measured, and various electronic, power, and control systems.

[0033] Referring to Figure 3A, the GCIB attenuation subsystem comprises a beam attenuator 302, and related actuators and controls. Beam attenuator 302 is (for example) a metal plate having a small circular attenuator aperture 303 through which an attenuated sample (attenuated GCIB 306) of the GCIB 128 can be made to pass. It is recognized that the attenuator

aperture 303 may (for example) be a small circular aperture or a rectangular slit aperture or even an array of circular apertures and can be an adjustable aperture such as an iris or adjustable slit. In a preferred, non-limiting embodiment, the attenuator aperture 303 is a circular knife edge hole with 1 millimeter diameter. Beam attenuator 302 is mounted rigidly to analyzer mounting and alignment plate 324 and is thereby electrically grounded and thermally heat sunk. Analyzer mounting and alignment plate 324 is connected by mechanical linkage 326 to mechanical actuator 328 to provide bi-directional actuation (in the direction of arrows 380) for inserting the beam attenuator 302 into the GCIB 128 with attenuator aperture 303 aligned with the GCIB axis 129 or for removing the GCIB attenuator subsystem entirely from the GCIB 128.

[0034] Continuing to refer to **Figure 3A**, the GCIB collimation subsystem comprises a beam attenuator 302, an attenuator aperture 303, and a beam collimator 304 having a collimator aperture 305, and related actuators and controls. Beam attenuator 302 and beam collimator 304 are mounted rigidly to analyzer mounting and alignment plate 324 and are thereby electrically grounded, thermally heat sunk, and maintained in alignment thereby. Attenuator aperture 303 and collimator aperture 305 are fixed in alignment by analyzer mounting and alignment plate 324 so as to be aligned substantially parallel with GCIB axis 129. It is recognized that the collimator aperture 305 may (for example) be a small circular aperture or a rectangular slit aperture or even an array of circular apertures and can be an adjustable aperture such as an iris or adjustable slit. Preferably the collimator aperture is the same shape (circular or slit) as is the attenuator aperture 303 and is of approximately equal size or smaller than the attenuator aperture 303. Thus the collimator aperture serves to collimate the attenuated GCIB 306 and to further attenuate the attenuated GCIB 306. In a preferred embodiment, the collimator aperture 305 is a circular knife edge hole with a diameter in the range of from 20 to 160 micrometers. Analyzer mounting and alignment plate 324 is connected by mechanical linkage 326 to mechanical actuator 328 to provide bi-directional actuation (in the direction of arrows 380) for inserting GCIB collimation subsystem into the GCIB 128 with attenuator aperture 303 and collimator aperture 305 both aligned with the GCIB axis 129 or for removing the GCIB collimation subsystem entirely from the GCIB 128. When the GCIB collimation subsystem is inserted, as shown in **Figure 3A**, beam attenuator 302

and beam collimator **304** transmit (respectively) an attenuated GCIB **306** and an attenuated and collimated GCIB **307**. Attenuated and collimated GCIB **307** is thus a sample of GCIB **128**.

[0035] Continuing to refer to **Figure 3A**, the GCIB switching subsystem comprises a beam attenuator **302**, an attenuator aperture **303**, a beam collimator **304** having a collimator aperture **305**, an electrostatic deflector plate **394**, and related actuators, power supplies and controls. Beam attenuator **302** and beam collimator **304** are mounted rigidly to analyzer mounting and alignment plate **324** and are thereby electrically grounded, thermally heat sunk, and maintained in alignment. Attenuator aperture **303** and collimator aperture **305** are fixed in alignment by analyzer mounting and alignment plate **324** so as to be aligned substantially parallel with GCIB axis **129**. Analyzer mounting and alignment plate **324** is connected by mechanical linkage **326** to mechanical actuator **328** to provide bi-directional actuation **380** for inserting GCIB collimation subsystem into the GCIB **128** with attenuator aperture **303** and collimator aperture **305** both aligned with the GCIB axis **129** for transmitting an attenuated and collimated sample (attenuated and collimated GCIB **307**) of GCIB **128** or for removing the GCIB collimation subsystem entirely from the GCIB **128**. An electrostatic deflector plate **394** is positioned proximal to and substantially parallel to attenuated GCIB **306** where GCIB **306** passes between beam attenuator **302** and beam collimator **304** and is rigidly fixed to analyzer mounting and alignment plate **324** by electrical insulating means not shown. Electrical lead **396** connects electrostatic deflector plate **394** to a beam gating controller **398** for conducting beam gating potentials from beam gating controller **398** to electrostatic deflector plate **394**. Beam gating controller **398** provides electrical signals to controllably deflect or not deflect attenuated GCIB **306** in the region between beam attenuator **302** and beam collimator **304**. It is realized that beam gating controller **398** can be remotely controlled by a higher level control system (not shown in this figure) for controllably providing deflection signals to electrostatic deflector plate **394**. By deflecting or not deflecting attenuated GCIB **306**, attenuated and collimated GCIB **307** may be gated off or on. Accordingly when the GCIB switching subsystem is inserted into GCIB **128**, it can form a beam switch for time-of-flight beam measurements as will be described in additional detail hereinafter.

[0036] Continuing to refer to **Figure 3A**, the GCIB energy spectrum measuring subsystem (energy spectrometer) comprises a beam attenuator **302**, an attenuator aperture **303**, a beam collimator **304**, a collimator aperture **305**, a grounded electrode **312**, an energy analyzer electrode **308**, an analyzing slit **318**, a current sensor **322**, and related actuators, power supplies and controls. The grounded electrode **312** has three apertures -- a first grounded electrode aperture **313** for admitting attenuated and collimated GCIB **307**, a second grounded electrode aperture **314** to permit transmission of the attenuated and collimated GCIB **307'**, and a third grounded electrode aperture **315** for transmitting an analyzed beamlet **316** (shown in **Figure 3B**). A beam energy analyzer comprises grounded electrode **312** and energy analyzer electrode **308**. The grounded electrode **312** and the energy analyzer electrode **308** are disposed at an angle (preferably approximately 45 degrees) to the path of the attenuated GCIB **306** (thus to the GCIB axis **129**). The grounded electrode **312** is rigidly fixed to the analyzer mounting and alignment plate **324** so is to be electrically grounded thereby. The energy analyzer electrode **308** is rigidly fixed to analyzer mounting and alignment plate **324** by electrical insulating means not shown. Electrical lead **336** connects energy analyzer electrode **308** to an analyzer power supply **386** for supplying an analyzer voltage V_{An} to energy analyzer electrode **308**. Analyzer power supply **386** is adjustable and preferably remotely controllable by a higher-level controller not shown in this figure. Analyzing voltage V_{An} is controllable throughout the range from zero to a voltage approximately equal to the maximum acceleration voltage V_{Acc} used for accelerating the GCIB **128**. For example if the maximum expected value of V_{Acc} is 25kV, then V_{An} can be chosen to be controllable over the range of from zero to 25kV. Energy analyzer electrode **308** has an energy analyzer electrode aperture **310** through the electrode to allow transmission of attenuated and collimated GCIB **307**. When transmitted through energy analyzer electrode aperture **310**, the continuation of attenuated and collimated GCIB **307** is designated as attenuated and collimated GCIB **307'**. Energy analyzer electrode aperture **310** is maintained in fixed alignment with attenuator aperture **303** and collimator aperture **305** by analyzer mounting and alignment plate **324**. When V_{An} is zero, the attenuated and collimated GCIB **307'** travels straight through attenuator aperture **303** and collimator aperture **305** and first grounded electrode aperture **313** and

through energy analyzer electrode aperture **310** and through second grounded electrode aperture **314**.

[0037] Referring to **Figure 3B**, but continuing discussion of the GCIB energy spectrum measuring subsystem (energy spectrometer), when V_{An} is greater than zero, an electrostatic field gradient exists between energy analyzer electrode **308** and grounded electrode **312** such that the attenuated and collimated GCIB **307** is deflected and dispersed, with cluster ions being dispersed as a function of their E/q (energy per charge). An analyzing slit **318** forms an acceptance aperture for a current sensor **322**, which is preferably a faraday cup having an electron suppressor electrode **320**. An electrical lead **330** connects suppressor electrode **320** to suppressor power supply **384** for supplying a suppressor voltage, V_{S1} to suppressor electrode **320** for suppressing secondary electrons in current sensor **322**. V_{S1} is preferably in the range of from **500** to **1500** volts. According to known principles, different values of V_{An} result in cluster ions of a specific range of energies, dependent on V_{An} , being deflected so as to pass through third grounded electrode aperture **315** and to form an analyzed beamlet **316** passing through analyzing slit **318** for measurement by the current sensor **322**. Cluster ions having E/q differing from the range of E/q of the cluster ions in analyzed beamlet **316** are deflected greater or lesser amounts than analyzed beamlet **316** and form dispersed beamlets **317**. Dispersed beamlets **317** do not pass through analyzing slit **318** and are not measured by current sensor **322**. Current sensor **322** has an electrical lead **332** for connecting it to a current measurement system **334**. According to known principles of electrostatic energy spectroscopy, by coordinating adjustment of V_{An} through its voltage range, with current measurements in current sensor **322** the energy spectrum (data in the form of beam current as a function of cluster ion energy or alternatively in the form of cluster ion energy as a function of beam current) of the attenuated and collimated GCIB **307** sample of GCIB **128** are measured and an average value of E/q (corresponding to $\left(\frac{E}{q}\right)_{average}$ in **Eqn. 3**) is calculated. Furthermore, the total cluster ion current, I , in the attenuated and collimated GCIB **307** can be obtained by integrating the measurement of beam current as a

function of cluster ion energy with respect to cluster ion energy. Such a measurement of cluster ion current, I , can be used in combination with a flow rate, Γ , measurement for calculating average charge state of the attenuated and collimated GCIB 307.

[0038] Referring again to **Figure 3A**, the GCIB particle flow measurement subsystem comprises a beam attenuator 302, an attenuator aperture 303, a beam collimator 304, a collimator aperture 305, an energy analyzer electrode aperture 310, a grounded electrode 342 with a fourth grounded electrode aperture 343, a dynode 338, an optional electron lens assembly 344, a scintillation measurement system, and related actuators, power supplies and controls. The GCIB particle flow measurement subsystem measures the flow rate Γ of clusters in a sample of the GCIB 100. Beam attenuator 302 and beam collimator 304 are mounted rigidly to analyzer mounting and alignment plate 324 and are thereby electrically grounded, thermally heat sunk, and maintained in alignment. Analyzer voltage V_{An} is set to zero so that attenuated and collimated GCIB 307 is transmitted through the energy analyzer electrode aperture 310 as attenuated and collimated GCIB 307'. Grounded electrode 342 with a fourth grounded electrode aperture, dynode 338, optional electron lens assembly 344, which if used, is preferably an einzel lens, scintillator 348, and a photomultiplier tube (PMT) 350 are all rigidly mounted to a particle detector mounting and alignment plate 352. When electron lens assembly is used, an electrical lead 358 connects electron lens assembly to lens power supply 388 for providing focusing voltage V_{L3} for focusing secondary electron trajectories 346 onto scintillator 348.

[0039] Particle detector mounting and alignment plate 352 supports and maintains alignment of elements mounted to it and permits their positioning, as a group. Particle detector mounting and alignment plate 352 is connected by mechanical linkage 362 to mechanical actuator 360 to provide bi-directional actuation (in the direction of arrows 382) for inserting the dynode 340 into the attenuated and collimated GCIB 307' for cluster ion flow rate measurement. The grounded electrode 342 is rigidly mounted to the particle detector and mounting plate 352 and is electrically grounded thereby. The dynode is rigidly mounted to the particle detector and mounting plate 352 by electrical insulating means not shown. Both the grounded electrode 342 and the dynode

are disposed at an angle (preferably approximately 45 degrees) to the path of the attenuated and collimated GCIB 307' (thus to the GCIB axis 129). Dynode 338 is an electrical conductor, preferably aluminum, and has a dynode surface 340, preferably a thin native aluminum oxide film. An electrical lead 364 connects the dynode 338 to a dynode power supply 390 for supplying a dynode voltage V_{Dy} to the dynode 338. Dynode power supply 390 is preferably remotely controllable by a higher level controller for setting V_{Dy} to zero volts when particle detection is not being performed and to set it to a fixed value, preferably in the range of 20-45 kV and typically 30 kV when particle detection is performed. In operation, attenuated and collimated GCIB 307' passes through fourth grounded electrode aperture 343 in the grounded electrode 342. An electric potential gradient between the dynode 338 and grounded electrode 342 accelerates the attenuated and collimated GCIB 307' into the dynode 338. As each accelerated cluster ion strikes the dynode surface 340, it induces release of one or more secondary electrons.

[0040] The secondary electrons are accelerated by the electric field gradient between the dynode 338 and the grounded electrode 342 along trajectories 346 in a direction substantially normal to the dynode surface 340 and are focused by electron lens assembly 344 onto a scintillator 348. The electron lens assembly 344 is optional, but is useful for assuring detection of electrons at the scintillator with a relatively small scintillator. Each cluster ion arriving at the dynode surface releases a burst of one or more secondary electrons, which is converted by the scintillator 348 to a photon pulse. Scintillator 348 is a conventional particle detecting scintillator known in the art (preferably a plastic scintillator). Scintillator 348 is shielded from external light sources by a thin aluminized Mylar film and is optically coupled to a high speed PMT 350. An electrical cable 354 connects PMT 350 to a conventional PMT controller/pulse counter/sampling system 356. The PMT controller/pulse counter/sampling system 356 provides and controls power supply potentials to the PMT and processes the PMT output pulses to provide pulse rate measurements and also processes the PMT output to collect periodic samples of the PMT output signal for measuring the fall-off of the signal during time-of-flight measurement, as further described hereinafter. The PMT 350 produces a pulse output corresponding to each photon pulse detected, thus corresponding to each cluster ion that strikes

the dynode surface **340**. PMTs capable of counting photon pulse rates of at least 100 MHz are commercially available. The PMT controller/pulse counter/sampling system **356** is remotely controllable and can output its pulse rate and sampling measurements for remote reading. The beam attenuator aperture **303** is pre-selected to have a diameter so as to provide an overall attenuation of the GCIB **128** as to assure that the cluster ion flow rate in the attenuated and collimated GCIB **107'** is at an accurately countable rate by the PMT **350**. For presently typical examples of GCIB **100** this attenuation factor is on the order of 10^{-6} to 10^{-7} , which can be achieved by using an attenuator aperture on the order of 20 micrometers diameter. The measured cluster ion flow rate in the attenuated and collimated GCIB **307'** is designated Γ , and corresponds to the Γ in **Eqn. 2**.

[0041] Continuing to refer to **Figure 3A**, a first example of a GCIB current measurement subsystem for implementing the invention comprises a grounded aperture **372**, a secondary electron suppressor **374**, and a beam current sensor **376**. The aperture **372**, secondary electron suppressor, and beam current sensor **376** are rigidly mounted (not shown here) so as to be aligned with the GCIB axis **129** of GCIB **128** (and thus also aligned with attenuated and collimated GCIB **307'**). In the absence of intervening elements, GCIB **128** or a sample of GCIB **128** (attenuated and collimated GCIB **307'**, for example) is collected by current sensor **376** for measurement. Current sensor **376** is preferably a faraday cup. An electrical lead **366** connects secondary electron suppressor **374** to a suppressor power supply **392** for supplying a suppressor voltage V_{S2} to the secondary electron suppressor **374** for suppressing secondary electrons in the current sensor **376**. V_{S2} is preferably in the range of from 500 to 1500 volts. An electrical lead **368** connects current sensor **376** to electrical current measuring system **370** for electrical current measurement.

[0042] Referring again to **Figure 3B**, a second and preferred example of a GCIB current measurement subsystem for implementing the invention utilizes the current sensor **322** (preferably a faraday cup) of the energy spectrum measuring subsystem for measuring the beam current, I , of the attenuated and collimated GCIB **307**. When V_{An} is greater than zero, an

electrostatic field gradient exists between energy analyzer electrode **308** and grounded electrode **312** such that the attenuated and collimated GCIB **307** is deflected and dispersed, with cluster ions being dispersed as a function of their E/q (energy per charge). An analyzing slit **318** forms an acceptance aperture for the current sensor **322**, which is preferably a faraday cup having an electron suppressor electrode **320**. An electrical lead **330** connects suppressor electrode **320** to suppressor power supply **384** for supplying a suppressor voltage, V_{SI} to suppressor electrode **320** for suppressing secondary electrons in current sensor **322**. V_{SI} is preferably in the range of from **500** to **1500** volts. By coordinating adjustment of V_{An} through its voltage range, with current measurements in current sensor **322** the energy spectrum (in the form of beam current as a function of cluster ion energy) of the attenuated and collimated GCIB **307** sample of GCIB **128** is measured and the cluster ion current, I , in the attenuated and collimated GCIB **307** can be obtained by integrating the measurement of beam current as a function of cluster ion energy with respect to cluster ion energy. Γ is the corresponding measured cluster ion flow rate in the attenuated and collimated GCIB **307**. Collection efficiencies α and β are determined by conventional calibration techniques and thus \bar{q} is calculated according to **Eqn. 2**. Average energy/charge, $\left(\frac{E}{q}\right)_{average}$ is also measured as described hereinbefore and accordingly \bar{E} is calculated according to **Eqn. 3**. Since attenuated and collimated GCIB **307'** is a sample of GCIB **128**, the calculated values of \bar{q} and \bar{E} correspond to those for GCIB **128**.

[0043] **Figure 4** shows a schematic **400** of the first embodiment of a GCIB measurement apparatus configured for making a sample beam current measurement using the first example GCIB current measurement subsystem. Mechanical actuator **360** removes the particle detector mounting and alignment plate **352** from the path of the attenuated and collimated GCIB **307'**, which is a sample of GCIB **128**. When the analyzer mounting and alignment plate **324** is positioned so that the GCIB attenuation and collimation subsystems are inserted into the GCIB **128** and the particle detector mounting and alignment plate **352** is removed from the path of attenuated and collimated GCIB **307'** (as shown in **Figure 4**), then the attenuated and collimated

GCIB 307', which is a sample of GCIB 128 is collected by the current sensor 376 for measurement as the sample beam current value I of Eqn. 2 is the current in the attenuated and collimated GCIB 307', while Γ is the corresponding measured cluster ion flow rate in the attenuated and collimated GCIB 307'. Collection efficiencies α and β are determined by conventional calibration techniques and thus \bar{q} is calculated according to Eqn. 2. Average energy/charge, $\left(\frac{E}{q}\right)_{average}$ is also measured as described hereinbefore and accordingly \bar{E} is calculated according to Eqn. 3. Since attenuated and collimated GCIB 307' is a sample of GCIB 128, the calculated values of \bar{q} and \bar{E} correspond to those for GCIB 128.

[0044] Figure 5 shows a schematic 410 of the first embodiment of the GCIB measurement apparatus of the invention, configured for gating a sample of the GCIB 128 for making time-of-flight measurements on the beam sample. The analyzer mounting and alignment plate 324 and the particle detector mounting and alignment plate 352 are both positioned so that the GCIB attenuation and collimation subsystems are inserted into the GCIB 128 and the particle detector mounting and alignment plate 352 is in the path of attenuated and collimated GCIB 307' (as was shown in Figure 3A). The time-of-flight measurement is done by beginning with the beam conditions shown in Figure 3A, with the attenuated and collimated GCIB 307' striking dynode 338 and being sensed by PMT 350. Referring again to Figure 5, beam gating controller 398 provides electrical signals to controllably deflect the attenuated GCIB 306 in the region between beam attenuator 302 and beam collimator 304. This results in attenuated GCIB 306 (Figure 3A) being deflected as attenuated and deflected GCIB 412 (Figure 5). The deflection results in abrupt gating off of the previously (as was shown in Figure 3A) attenuated and collimated GCIB 307 – 307', which results in a delayed (according to the times-of-flight of the component clusters having various energies in the attenuated and collimated GCIB 307 – 307') fall-off of signal in the PMT 350. The electrical cable 354 connects PMT 350 to PMT controller/pulse counter/sampling system 356 for measuring the delayed fall-off signal in the PMT 350, which occurs after the gating off of the attenuated and collimated GCIB 307 - 307'.

[0045] A time-of-flight analysis and control system 414 is controllably connected to both the beam gating controller 389 and the PMT controller/pulse counter/sampling system 356 by electrical cables 416 and 418 respectively. The time-of-flight analysis and control system 414 also receives measurement information about the delayed fall-off signal in the PMT 350 via the electrical cable 418. The process for measuring cluster ion time-of-flight begins with the GCIB measurement apparatus 300 configured as shown in the previous Figure 3A, with attenuated and collimated GCIB 307' being collected by the beam current sensor 376. The time-of-flight analysis and control system 414 sends control signals to the PMT controller/pulse counter/sampling system 356 to cause it to collect and send periodic samples of the signal sensed at PMT 350. At a time T_0 , the time-of-flight analysis and control system 414 sends control signals to beam gating controller 398 commanding the attenuated and collimated GCIB 307' to be gated off, as shown in Figure 5. The resulting fall-off of signal at beam PMT 350 is periodically sampled and sent to the time-of-flight analysis and control system 414 by the PMT controller/pulse counter/sampling system 356. The rate and timing of the fall-off of signal at the PMT 350 is analyzed in relation to the time T_0 of beam gating by the beam gating controller 398 according to principles as taught in US patent application publications 2002-0036261A1, Dykstra; and 2002-0070361A1, Mack *et al.*, for example. US patent application publications 2002-0036261A1, Dykstra; and 2002-0070361A1, Mack *et al.* are incorporated herein by reference. Accordingly, the time-of-flight distribution for the attenuated and collimated GCIB 307 – 307' is measured. By conventional averaging techniques, the average time-of-flight is calculated from the time-of-flight distribution and the average velocity, \bar{v} , is the inverse of the average time-of-flight. This calculated value of average velocity \bar{v} is the value \bar{v} for Eqn. 5. By combining this value of \bar{v} with the value of \bar{E} calculated according to Eqn. 3, next is calculated the value of average mass \bar{m} according to Eqn. 5. Therefore, according to the methods and apparatus of the first embodiment of the invention, average mass \bar{m} , average velocity \bar{v} , average energy \bar{E} , average charge state \bar{q} , and average energy/charge $\left(\frac{E}{q}\right)_{average}$ are determined for the sample of the beam and therefore for the GCIB

128. It is recognized that the time-of-flight analysis and control system **414** could optionally be implemented as part of a higher level or more general control system, a microcomputer system, or other general-purpose computer system, which might be part of an overall control system for a GCIB processing system.

[0046] **Figure 6** shows a schematic **420** of the first embodiment of the GCIB measurement apparatus of the invention, but with the measurement improvements removed from the beam path to permit measurement of the current of the entire GCIB **128**. The analyzer mounting and alignment plate **324** is positioned so that the subsystems it supports are removed entirely from the GCIB **128** and the particle detector mounting and alignment plate **352** is also positioned so that the subsystems it supports are removed entirely from the GCIB **128**. GCIB **128** travels uninterrupted to the current sensor **376** where it is collected for measurement. This permits measurement of total beam current I_T of the GCIB **128** for workpiece processing dosimetry purposes.

[0047] **Figure 7** shows a schematic of a second embodiment of a GCIB measurement apparatus **430** for making the beam measurements of the invention upon a GCIB **128**. In the second embodiment, the method does not include a time-of-flight measurement, but rather makes

measurements of average mass per charge $\left(\frac{m}{q}\right)_{average}$ of the beam, and of average energy per

charge $\left(\frac{E}{q}\right)_{average}$, and average charge state \bar{q} on a sample of the cluster ion beam. The average

energy per charge and the average charge state are measured identically and with the same apparatus as used for the first embodiment and as has been described hereinbefore. The average mass per charge is measured using a pressure-charge sensor, according to known techniques. The measurement apparatus is like the apparatus of the first embodiment described hereinbefore, except that since no time-of-flight measurement is required, the previously described electrostatic deflector plate **394**, electrical lead **396**, and beam gating controller **398** of the GCIB switching subsystem are not required. Also the separate secondary electron suppressor **374**, the beam

current sensor 376, electrical lead 368 and current measuring system 370 previously described are not required. Beam current measurement and average mass per charge are performed using apparatus and methods as are now described. A (m/q) sensor 432 comprises a perforated faraday cup 434 with a secondary electron suppressor 436 and a pressure sensor 442. The grounded aperture 372 and (m/q) sensor 432 are rigidly mounted (not shown here) so as to be aligned with the GCIB axis 129 of GCIB 128. In the absence of intervening elements, the perforated faraday cup 434 collects GCIB 128 for current measurement. Gas cluster ions in the GCIB 128 are fully dissociated upon impact with the perforated faraday cup 434 and they raise the pressure in the (m/q) sensor 432 as they escape. Pressure sensor 442 measures the pressure increase due to dissociated gas cluster ions and measures the temperature of the sensor. An electrical lead 366 connects secondary electron suppressor 436 to a suppressor power supply 392 for supplying a suppressor voltage V_{s2} to the secondary electron suppressor 374 for suppressing secondary electrons in the perforated faraday cup 434. V_{s2} is preferably in the range of from 500 to 1500 volts. An electrical lead 448 connects perforated faraday cup to a conventional current measurement system 446 for electrical current measurement. An electrical cable 438 connects pressure sensor 442 to a (m/q) measurement system 440 for transmitting pressure and temperature signals and sensor power. An electrical lead 444 transmits electrical current measurement signals from current measurement system 446 to the (m/q) measurement system 440. The current measurement system 446 and the (m/q) measurement system 440 are both remotely controllable and able to provide data signals to a higher-level controller, not shown here. The (m/q) sensor 432, the current measurement system 446, and the (m/q) measurement system 440 operate according to principles taught in US patent application publication 2001-0054686A1 Torti *et al.*, for example. US patent application publication 2001-0054686A1 Torti *et al.* is incorporated herein by reference. Equation 10 of 2001-0054686A1 Torti *et al.* describes the measurement for \bar{N} , the average number of molecules per cluster. By multiplying \bar{N} , thus obtained, by 40 (the atomic mass of Argon) and by the value of the atomic mass unit in kg, is

obtained the value of average mass per charge $\left(\frac{m}{q}\right)_{average}$, for the clusters in the GCIB 128. This value for average mass per charge is the $\left(\frac{m}{q}\right)_{average}$ required in Eqn. 4. The current measurement of the GCIB 128 from the current measurement system 446 is I_T , the total beam current for the GCIB 128 and is used for GCIB processing dosimetry. By combining this value for average mass per charge with measurements of Γ , I , and average energy per charge $\left(\frac{E}{q}\right)_{average}$, obtained according to the methods and apparatus of the first embodiment of the invention described above, and by applying Eqn. 2, Eqn. 3, and Eqn. 4, average mass \bar{m} , average charge state \bar{q} , and average energy \bar{E} are determined for the GCIB 128 according to the second embodiment of the invention.

[0048] Figure 8 shows a schematic 450 of the first embodiment of the GCIB measurement apparatus of the invention, but with the measurement improvements removed from the beam path to permit processing of a workpiece by GCIB irradiation using the entire GCIB 128. The analyzer mounting and alignment plate 324 is positioned so that the subsystems it supports are removed entirely from the GCIB 128 and the particle detector mounting and alignment plate 352 is also positioned so that the subsystems it supports are removed entirely from the GCIB 128 and from the scanning path of a mechanically scanning workpiece holder 150 with a workpiece 152. GCIB 128 travels uninterrupted to the workpiece 152 where it irradiates the workpiece for GCIB processing of the workpiece 152. The workpiece holder 150 and workpiece 152 are scanned through the GCIB 128 with X-scan and Y-scan motions 208 and 210, using apparatus and methods equivalent to those previously described in more detail in the discussion of the mechanically scanning GCIB processing apparatus 200 (see discussion of Figure 2, hereinbefore).

[0049] Figure 9 is a schematic showing an improved GCIB measurement and processing apparatus 500 according to a preferred first embodiment of the invention. GCIB measurement

and processing apparatus **500** is similar to the prior art mechanically scanning GCIB processing apparatus **200**, but having GCIB measurement, monitoring, and control improvements for implementing the first embodiment of the invention. Gas metering valve **113** of the prior art processing system is replaced by electronically controllable gas metering valve **512**. The beam current sensor **218** of the prior art system and its electrical lead **214** are replaced by aperture **372**, secondary electron suppressor **374**, beam current sensor **376**, and electrical lead **368** of the hereinbefore described GCIB measurement apparatus **300**. Controller **220** of the prior art system is replaced by digital processing and control system **510** having improved capabilities and functions, including but not limited to all the hereinbefore described functionality of controller **220** and time-of-flight analysis and control system **414**. Digital processing and control system **510** also includes the capability to control analyzer power supply **386** and to receive signals from current measurement system **334** and to coordinate adjustment of V_{an} with measurement of current signals from current sensor **322** to perform beam energy spectrum measurement, with data in the form of beam current as a function of cluster ion energy or alternatively in the form of cluster ion energy as a function of beam current, of the attenuated and collimated GCIB **307** sample of GCIB **128** and to integrate the measurement of beam current as a function of cluster ion energy with respect to cluster ion energy to determine the cluster ion current, I , in the attenuated and collimated GCIB **307**.

[0050] Digital processing and control system **510** may be, for example, a small general-purpose computer for general control of a GCIB processing system. Digital processing and control system **510** has a control bus **504** for communicating with and controlling other devices and/or subsystems. Anode power supply **134**, filament power supply **136**, and accelerator power supply **140** are each equipped with remote control capabilities and are controllably connected to the digital processing and control system **510** for control thereby via control bus **504**. Electronically controllable gas metering valve **512** is also controllably connected to the digital processing and control system **510** for control thereby via control bus **504**. Electrical lead **508** connects current measurement system **334** with digital processing and control system **510** for transmitting current measurement signals from current sensor **322**. The improved GCIB

measurement and processing apparatus **500** additionally incorporates all of the elements of the hereinbefore-described GCIB measurement apparatus **300**. Digital processing and control system **510** communicates with and controls (via control bus **504**) at least the following devices: suppressor power supply **384**, for switching V_{S1} on or off; the beam gating controller **398** for sending beam gating commands; mechanical actuators **328** and **360** for commanding positioning of (respectively) analyzer mounting and alignment plate **324** and particle detector mounting and alignment plate **352** with respect to GCIB axis **129**; anode power supply **134**, for controlling V_A ; filament power supply **136**, for controlling V_F ; accelerator power supply **140**, for controlling V_{Acc} ; electronically controllable gas metering valve **512**, for controlling source gas **112** flow through nozzle **110** and/or source gas pressure in stagnation chamber **116**; analyzer power supply **386**, for controlling V_{An} ; optionally, if included, lens power supply **388** for controlling V_{L3} ; dynode power supply **390**, for controlling V_{Dy} ; suppressor power supply **392**, for switching V_{S2} on or off; and PMT controller/pulse counter/sampling system **356** for controlling supply voltages for PMT **350** and for enabling or disabling pulse detection and signal sampling by PMT **350** and for controlling transmission of pulse count (Γ measurement) information from PMT controller/pulse counter/sampling system **356** to **510** via electrical lead **506**. The digital processing and control system **510** controllably connects to the X-scan actuator **202** and the Y-scan actuator **204** through electrical cable **216** and controls the X-scan actuator **202** and the Y-scan actuator **204** so as to place the workpiece **152** into or out of the path of GCIB axis **129** and can remove the workpiece holder **150** to a position, as shown in **Figure 9**, where it does not collide with nor interfere with the function of components mounted on particle detector mounting and alignment plate **352**. When the analyzer mounting and alignment plate **324**, the particle detector mounting and alignment plate **354**, and the workpiece holder **152** are positioned as shown in **Figure 9**, then $\left(\frac{E}{q}\right)_{average}$ and Γ are measured by the digital processing and control system **510** according to the methods hereinbefore-described. When the digital processing and control system **510** commands retraction of the particle detector mounting and alignment plate

352 from the GCIB axis 129, the configuration shown in **Figure 4** is obtained and beam current value I is measured according to the method hereinbefore-described. Using the configuration shown in **Figures 4** and **5**, the digital processing and control system **510** commands beam gating controller **398** to gate the beam off and measures the average velocity \bar{v} by time of methods hereinbefore-described. Digital processing and control system **510** calculates \bar{q} according to **Eqn. 2**, and calculates \bar{E} according to **Eqn. 3**, and calculates \bar{m} according to **Eqn. 5**.

[0051] **Figure 10** is a schematic **550** showing the improved GCIB measurement and processing apparatus according to the preferred first embodiment of the invention, with the beam measurement apparatus removed from the beam to allow workpiece processing. As shown, both the analyzer mounting and alignment plate **324** and the particle detector mounting and alignment plate have been retracted from the path of the GCIB **128** by command of the digital processing and control system **510**. A workpiece **152**, which may be a semiconductor wafer, is held by workpiece holder **150**. Workpiece holder is manipulated by the X-scan actuator **202** and the Y-scan actuator **204** under control of the digital processing and control system **510** so as to place the workpiece **152** into or out of the path of GCIB **128** and to scan the workpiece **152** uniformly relative to the GCIB **128** to achieve uniform processing of the workpiece **152** by the GCIB **128**. Controller **510** receives the sampled beam current collected by the beam current sensor **376** by way of lead **368** and current measuring system **370** and thereby monitors the GCIB **128** and controls the GCIB dose received by the workpiece **152** by removing the workpiece **152** from the GCIB **128** when a predetermined desired dose has been delivered. Prior to initiation of processing of a workpiece by GCIB, desired target values or limiting values for any or all of \bar{E} , I_T , \bar{m} and \bar{q} are chosen and stored within the digital processing and control system **510**. For the GCIB parameters for which target or limiting values are stored, the digital processing and control system **510** measures those GCIB parameters on the GCIB **128** as described hereinbefore. Any GCIB parameters that are measured as not in compliance with the stored limits or targets are adjusted under control of the digital processing and control system **510**. \bar{E} is adjusted, for example, by adjusting V_{Acc} . I_T is adjusted, for example, by adjusting electronically

controllable gas metering valve **512** and/or by adjusting V_A and/or by adjusting V_F . \bar{m} is adjusted, for example, by adjusting electronically controllable gas metering valve **512**. \bar{q} is adjusted, for example, by adjusting V_A and/or V_F . When GCIB parameters, for which desired target values or limiting values have been stored, have all been obtained by automatic adjustment, the digital processing and control system **510** proceeds with the processing of the workpiece **152**. The digital processing and control system **510** monitors and, if necessary adjusts, GCIB parameters for which desired target values or limiting values have been stored prior to the processing of each workpiece. If the digital processing and control system **510** is unable, by system adjustments, to achieve the stored beam target or limit values, it halts processing and signals (through display means, not shown) a human operator, thus avoiding mis-processing of the workpiece or workpieces.

[0052] **Figure 11** is a schematic showing an improved GCIB measurement and processing apparatus **600** according to a preferred second embodiment of the invention. GCIB measurement and processing apparatus **600** is similar to the prior art mechanically scanning GCIB processing apparatus **200**, but having GCIB measurement, monitoring, and control improvements for implementing the second embodiment of the invention. Gas metering valve **113** of the prior art processing system is replaced by electronically controllable gas metering valve **512**. The beam current sensor **218** of the prior art system and its electrical lead **214** are replaced by aperture **372**, (m/q) sensor **432** and electrical lead **448**. Controller **220** of the prior art system is replaced by digital processing and control system **510** having improved capabilities and functions, including but not limited to all the hereinbefore described functionality of controller **220**. Digital processing and control system **510** may be, for example, a small general-purpose computer for general control of a GCIB processing system. Digital processing and control system **510** has a control bus **504** for communicating with and controlling other devices and/or subsystems. Anode power supply **134**, filament power supply **136**, and accelerator power supply **140** are each equipped with remote control capabilities and are controllably connected to the digital processing and control system **510** for control thereby via control bus **504**. Electronically controllable gas

metering valve **512** is also controllably connected to the digital processing and control system **510** for control thereby via control bus **504**. The improved GCIB measurement and processing apparatus **500** additionally incorporates all of the elements of the hereinbefore-described GCIB measurement apparatus **300**, except that the previously described electrostatic deflector plate **394**, electrical lead **396**, and beam gating controller **398** of the GCIB switching subsystem are not used. Also the separate secondary electron suppressor **374**, the beam current sensor **376**, electrical lead **368** and current measuring system **370** previously described are not used. The (m/q) sensor **432** comprises a perforated faraday cup **434** with a secondary electron suppressor **436** and a pressure sensor **442**. An electrical lead **448** connects perforated faraday cup to a conventional current measurement system **446** for electrical current measurement. An electrical cable **438** connects pressure sensor **442** to a (m/q) measurement system **440** for transmitting pressure and temperature signals and sensor power. An electrical lead **444** transmits electrical current measurement signals from current measurement system **446** to the (m/q) measurement system **440**. The current measurement system **446** and the (m/q) measurement system **440** are both remotely controllable and able to provide data signals to digital processing and control system **510**.

[0053] The digital processing and control system **510** communicates with and controls (via control bus **504**) at least the following devices: suppressor power supply **384**, for switching V_{S1} on or off; mechanical actuators **328** and **360** for commanding positioning of (respectively) analyzer mounting and alignment plate **324** and particle detector mounting and alignment plate **352** with respect to GCIB axis **129**; anode power supply **134**, for controlling V_A ; filament power supply **136**, for controlling V_F ; accelerator power supply **140**, for controlling V_{Acc} ; electronically controllable gas metering valve **512**, for controlling source gas **112** flow through nozzle **110** and/or source gas pressure in stagnation chamber **116**; analyzer power supply **386**, for controlling V_{An} ; optionally, if included, lens power supply **388**, for controlling V_{L3} ; dynode power supply **390**, for controlling V_{Dy} ; suppressor power supply **392**, for switching V_{S2} on or off; (m/q) measurement system **440**, for controlling pressure sensor power and for commanding (m/q) measurement and transmission; and PMT controller/pulse counter/sampling system **356** for

controlling supply voltages for PMT 350 and for enabling or disabling pulse detection by PMT 350 and for controlling transmission of pulse count (Γ measurement) information from PMT controller/pulse counter/sampling system 356 to 510 via electrical lead 506. Current measurement system 446 supplies total beam current I_T measurement signals to (m/q) measurement system 440 via electrical lead 444 and also to digital processing and control system 510 via electrical lead 604. (m/q) measurement system 440 provides (m/q) measurement signals to digital processing and control system 510 via electrical lead 602. The digital processing and control system 510 controllably connects to the X-scan actuator 202 and the Y-scan actuator 204 through electrical cable 216 and controls the X-scan actuator 202 and the Y-scan actuator 204 so as to place the workpiece 152 into or out of the path of GCIB axis 129 and can remove the workpiece holder 150 to a position as shown to facilitate GCIB 128 total beam current I_T measurement or to facilitate other GCIB parameter measurements. The digital processing and control system 510 commands the analyzer mounting and alignment plate 324, the particle detector mounting and alignment plate 354, and the workpiece holder 152 into positions analogous to those shown in Figure 9, and then $\left(\frac{E}{q}\right)_{average}$ and Γ are measured by the digital processing and control system

510 according to the methods hereinbefore-described. The digital processing and control system 510 commands the analyzer mounting and alignment plate 324, the particle detector mounting and alignment plate 354, and the workpiece holder 152 into positions as shown in Figure 11 and I_T and (m/q) are measured according to the methods hereinbefore-described. The digital processing and control system 510 calculates \bar{q} according to Eqn. 2, and calculates \bar{E} according to Eqn. 3, and calculates \bar{m} according to Eqn. 4. As shown in Figure 11, both the analyzer mounting and alignment plate 324 and the particle detector mounting and alignment plate have been retracted from the path of the GCIB 128 by command of the digital processing and control system 510 for workpiece processing by GCIB irradiation. A workpiece 152, which may be a semiconductor wafer, is held by workpiece holder 150. Workpiece holder is manipulated by the X-scan actuator 202 and the Y-scan actuator 204 under control of the digital processing and control system 510

so as to place the workpiece **152** into or out of the path of GCIB **128** and to scan the workpiece **152** uniformly relative to the GCIB **128** to achieve uniform processing of the workpiece **152** by the GCIB **128**. Controller **510** receives the sampled beam current collected by the perforated faraday cup **434** by way of lead **448** and current measuring system **446** and electrical lead **604** and thereby monitors the GCIB **128** total beam current I_T and controls the GCIB dose received by the workpiece **152** by removing the workpiece **152** from the GCIB **128** when a predetermined desired dose has been delivered.

[0054] Prior to initiation of processing of a workpiece by GCIB, desired target values or limiting values for any or all of \bar{E} , I_T , \bar{m} and \bar{q} are chosen and stored within the digital processing and control system **510**. For the GCIB parameters for which target or limiting values have been stored, the digital processing and control system **510** measures those GCIB parameters on the GCIB **128** as described hereinbefore. Any GCIB parameters that are measured as not in compliance with the stored limits or targets are adjusted under control of the digital processing and control system **510**. \bar{E} is adjusted, for example, by adjusting V_{Acc} . I_T is adjusted, for example, by adjusting electronically controllable gas metering valve **512** and/or by adjusting V_A and/or by adjusting V_F . \bar{m} is adjusted, for example, by adjusting electronically controllable gas metering valve **512**. \bar{q} is adjusted, for example, by adjusting V_A and/or V_F . When GCIB parameters, for which desired target values or limiting values have been stored, have all been obtained by automatic adjustment, the digital processing and control system **510** proceeds with the processing of the workpiece **152**. The digital processing and control system **510** monitors and, if necessary, adjusts GCIB parameters for which desired target values or limiting values have been stored prior to the processing of each workpiece. If the digital processing and control system **510** is unable, by system adjustments, to achieve the stored beam target or limit values, it halts processing and signals (through display means, not shown) a human operator, thus avoiding mis-processing of the workpiece or workpieces.

[0055] Although the invention has been described with respect to measurement of gas cluster ion beams, it is recognized by the inventor that the invention is also applicable to measurement of

parameters of cluster ion beams that do not comprise source materials that are gaseous under conditions of standard temperature and pressure and thus is useful in the more general case of measurement of cluster ion beams, including gas cluster ion beams and non-gas cluster ion beams such as, for example, metal cluster ion beams. It is further recognized by the inventor that the invention is useful for measuring parameters of molecular ion beams comprising very heavy molecules. Although the invention has been described with respect to various embodiments, it should be realized this invention is also capable of a wide variety of further and other embodiments within the spirit of the invention.

[0056] I claim: